

[cylindrical detector efficiency]  
 (Chapter 8.2.1 in *Elements*)

### Efficiency of a cylindrical detector

Assuming a uniform incoming neutron beam and averaging over one-half of the detector diameter, the efficiency is

$$\varepsilon(\lambda) = \frac{1}{R} \int_0^R dz \int_{y_{\min}}^{y_{\max}} \exp(-N\sigma(y - y_{\min})) dy, \quad (8-CDE-$$

1)

in which  $z$  is measured perpendicular to the axis of the detector and  $R$  is the radius of the cylinder, as in Figure 8-CDE-1.

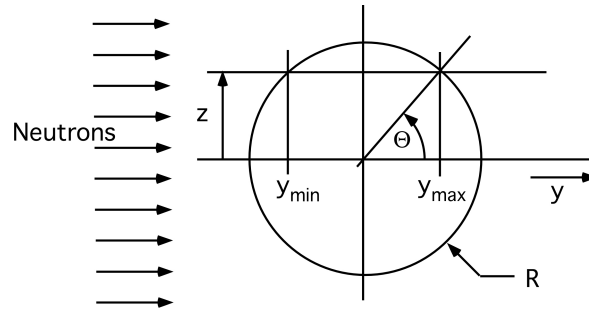


Figure 8-CDE-1 Neutron paths in a cylindrical detector.

Taking  $z = R \sin(\theta)$ ,  $y_{\min} = -R \cos(\theta)$ , and  $y_{\max} = R \cos(\theta)$ , the expression becomes

$$\varepsilon(\lambda) = 1 - \int_0^{\pi/2} \exp(-2N\sigma R \cos(\theta)) \cos(\theta) d\theta. \quad (8-CDE-$$

1)

A useful series representation results from expanding the exponential in a power series,

$$\varepsilon(\lambda) = \sum_{n=1}^{\infty} \frac{(-1)^{n+1} X^n}{n!} Z_n, \quad (8-CDE-$$

2)

where

$$X = 2N\sigma(\lambda)R \quad (8-CDE-$$

3)

and

$$Z_n = \frac{\sqrt{\pi}}{2} \frac{\Gamma\left(\frac{n}{2}+1\right)}{\Gamma\left(\frac{n}{2}+\frac{3}{2}\right)} = \begin{cases} \frac{\pi}{4}, \frac{3\pi}{4}, \frac{5\pi}{32}, \dots & \text{for } n = 1, 3, 5, \dots = 2p+1; \\ \frac{2}{3}, \frac{8}{15}, \frac{48}{105}, \dots & \text{for } n = 2, 4, 6, \dots = 2p \end{cases} \quad (8\text{CDE-})$$

4)

The coefficients are easily generated recursively from  $Z_0 = 1$  and  $Z_1 = \frac{\pi}{4}$ ,

$$Z_n = \frac{p+1/2}{p+1} Z_{n-2} \text{ for } n = 1, 3, 5, \dots = 2p+1 \text{ and} \quad (8\text{-CDE-})$$

5)

$$Z_n = \frac{p}{p+1/2} Z_{n-2} \text{ for } n = 2, 4, 6, \dots = 2p. \quad (8\text{-CDE-})$$

6)

The series converges for all  $X$ . When the magnitude of successive terms is diminishing with increasing  $N$ , the absolute error after summing  $N$  terms is

$$|\Delta\varepsilon| \leq \frac{X^{N+1}}{(N+1)!} Z_{N+1}. \quad (8\text{-CDE-})$$

7)

The limits for large and small  $X$  can be inferred from inspection of the starting expression,

$$\lim_{X \rightarrow 0} |\Delta\varepsilon(X)| = \pi \frac{X}{4} \text{ and } \lim_{X \rightarrow \text{large}} |\Delta\varepsilon(X)| = 1. \quad (8\text{-CDE-})$$

8)

A method for rapid calculation of CDEindrical counter efficiency, Carpenter 1981, based on a series expansion of a correction of the first-order result, , a mean-chord approximation.

$$\varepsilon(\lambda) \approx 1 - \exp\left(-\frac{\pi}{4} X\right). \quad (8\text{-CDE-})$$

9)

The full series expression is

$$1 - \varepsilon(\lambda) = \exp\left(-\frac{\pi}{4} X\right) \left( \sum_{m=0}^M \left(\frac{\pi}{4} X\right)^m Y_m + R_M \right), \quad (8\text{-CDE-10})$$

where

$$Y_m = \sum_{n=0}^m \frac{1}{n!(m-n)!} \left(-\frac{\pi}{4}\right)^n Z_n, \quad (8-CDE-11)$$

in which the  $Z_n$  s are as above. The  $Z_n$  and  $Y_m$  are independent of  $X$ , therefore, independent of wavelength and geometry, that is, universal for all detector sizes and all wavelengths, and are tabulated in IPNS Note 17. The remainder after  $M$  terms is  $R_M$ , which is bounded by

$$R_M \leq \left(\frac{\pi}{4} X\right)^{M+1} \frac{Y_{M+1}}{1-r_M}, \quad (8-CDE-12)$$

in which

$$r_m = \left(\frac{\pi}{4} X\right) \frac{Y_{m+1}}{Y_m} \quad (8-CDE-13)$$

is the ratio of successive terms in the  $Y$ -expansion.

The mean position of detection,  $\bar{y}$ , measured from the cylindrical axis, is

$$\bar{y} = \frac{1}{N\sigma(\lambda)} + \frac{\pi R}{4} \left[1 + \frac{\xi - 2}{\varepsilon(\lambda)}\right], \quad (8-CDE-14)$$

where

$$\xi = \sum_{m=1}^{\infty} m \left(\frac{X\pi}{4}\right)^{m-1} Y_m. \quad (8-CDE-15)$$

Therefore the mean time of detection, measured from the time of crossing the detector axis, is

$$\bar{t} = \frac{\bar{y}}{v}, \quad (8-CDE-16)$$

where  $v$  is the neutron speed. Always,  $\bar{y}$  and  $\bar{t}$ , are less than zero.

## Reference

Carpenter, J. M. (1981). Efficient code for calculating cylindrical gas proportional counter efficiency, unpublished technical note IPNS Note #17.